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Pipe Stress Engineering. Ed. Peng, L, & Peng, T. ASME Press, 2009. A piping system is the most efficient and common means of transporting fluids from one point to another. Within a petrochemical complex, acres and acres of piping can be seen running in every direction and at many different levels. Piping constitutes 25% to 35% of the material ...

Peng, L, & Peng, T. "Flexible Connections." Pipe Stress Engineering. Ed. Peng, L, & Peng, T. ASME Press, 2009. In Chapter 3, we discussed thermal expansion and piping flexibility. A piping system has to be flexible enough to absorb the thermal expansion displacement, without creating unacceptable stresses in the pipe or excessive reaction loads ...

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Proceedings of the ASME 2003 International Mechanical Engineering Congress and Exposition. Recent Advances in Mechanics of Solids and Structures. Washington, DC, USA. November 15–21, ... Pipes, Stress. This content is only available via PDF.

22/12/2008 · "The Stress Analysis and Residual Stress Evaluation of Pressure Armour Layers in Flexible Pipes Using 3D Finite Element Models." Proceedings of the ASME 2004 23rd International Conference on Offshore Mechanics and Arctic Engineering. 23rd International Conference on Offshore Mechanics and Arctic Engineering, Volume 3.

12/5/2008 · Sano, T, & Naoi, H. "Deformation Behavior of Intrusion Bending for Steel Pipes." Proceedings of the ASME 2003 International Mechanical Engineering Congress and Exposition . Applied Mechanics and Biomedical Technology .

12/5/2008 · The maximum pipe stresses were then compared to the fatigue stresses of the pipes, and the failure mechanisms were thus established. By slowly closing valves, the effects of the fluid transient can

be nearly eliminated. Using the closed from equations, the minimum time of valve closure may be calculated to prevent recurrent pipe failures.

2/10/2008 · Plastics pipes fail as a consequence of such movements, though their flexibility can make them less vulnerable than rigid pipes. This paper presents two extreme case studies of failure; a 100mm diameter polyvinyl chloride (PVC) domestic sewer pipe and 2700mm diameter glass reinforced plastic (GRP) intake pipeline.

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8/8/2013 · The results of the real measurements of the cross section form of different pipes are presented. The general approach for treating the out-of-roundness is given and an example of measurement of real pipe cross-section is presented. The stress calculation part of the procedure is based on the results presented in work [2].

22/12/2008 · "The Stress Analysis and Residual Stress Evaluation of Pressure Armour Layers in Flexible Pipes Using 3D Finite Element Models." Proceedings of the ASME 2004 23rd International Conference on Offshore Mechanics and Arctic Engineering. 23rd International Conference on Offshore Mechanics and Arctic Engineering, Volume 3.

12/5/2008 · The maximum pipe stresses were then compared to the fatigue stresses of the pipes, and the failure mechanisms were thus established. By slowly closing valves, the effects of the fluid transient can be nearly eliminated. Using the closed from equations, the minimum time of valve closure may be calculated to prevent recurrent pipe failures.

29/7/2008 · This behavior is consistent with the B31.1 and ASME Section III Class 2 and 3 piping paragraphs on “Local Overstrain”. The implication from this work is that the safety factor on secondary stresses in the ASME Section XI Code pipe flaw evaluation procedures should be a function of the failure stress.

15/1/2021 · The results indicated that the depth of soil support is a dominant factor for the pipe stress and deflection during an integrity excavation, which has not been previously investigated. Significant axial stress and strain in the longitudinal direction were produced by excavation, which may increase the risk of failure for the pipe that is suspected of circumferential defects.

10/11/2016 · In this paper, a methodology is presented to develop load factors for use in elastic-plastic assessments of pipelines and their components. The load factors are based on the pipe material properties and the ASME pipeline code’s design margin for the service and location of the pipeline installation [1, 2].

26/10/2017 · Research has shown that estimating local stress is important near the shoe support tip especially for large diameter piping systems and aboveground pipelines. To evaluate protection against local failure under an applied design load, a more accurate estimation method of ASME Sec. VIII Div.2, part 5 is applied by using elastic-plastic stress analysis procedures.

12/8/2008 · Klumpp, PT. "Expander Inlet Piping Design." Proceedings of the ASME/JSME 2004 Pressure Vessels and Piping Conference.Design and Analysis of Pressure Vessels, Heat Exchangers and Piping …

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17/1/2014 · Despite the availability of special purpose FE codes with post processing facilities as per rules of ASME SEC VIII Division 2, use of simple analytical methods like ring loading around a circumference or more complex methods like Welding Research council bulletins 107 and 297, will continue to be used in the industry for a significant period of time for stress analysis of pipe support …

9/7/2010 · Based on the Taguchi orthogonal array, finite element simulations are carried out to obtain the seismic code stress in each piping system. From the Taguchi signal-to-noise (S/N) ratio analysis and the analysis of variance (ANOVA) of the seismic code stress results, the effect of FRS and SAM on the resultant seismic stress is given and expressed as a percentage.

29/7/2008 · This behavior is consistent with the B31.1 and ASME Section III Class 2 and 3 piping paragraphs on “Local Overstrain”. The implication from this work is that the safety factor on secondary stresses in the ASME Section XI Code pipe flaw evaluation procedures should be a function of the failure stress.

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12/8/2008 · "ASME Section III Design-by-Analysis Criteria Concepts and Stress Limits." Proceedings of the ASME/JSME 2004 Pressure Vessels and Piping Conference . Design and Analysis of Pressure Vessels, Heat Exchangers and Piping Components .

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12/8/2008 · That is, a 1.5S m [2] check on membrane stress intensities arising from thermal piping loads is typically not performed. The key assumption used in support of this approach has been that these loads decay appreciably with local shell deformation such that the associated stresses are truly self-limiting in nature.

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